1. Introduction

This application note provides a brief overview about the possible ESD protecting realizations for any Silicon Labs RF designs. However, experimental measurements have only been taken with, and thus the efficiency of the ESD protection realizations has been demonstrated on, Si4x6x-based reference designs.

RF radio chips are designed for and tested against the different chip-level ESD standards such as Human Body Model (HBM), Machine Model (MM) and Charged Device Model (CDM). These chip-level test results are summarized in the RF IC's Qualification Report.

However, in a real-world application the final module has to resist and stand against an ESD shock. For this purpose, the final electronic product has to be tested against a different, more stringent standard that simulates and replicates the real world ESD stress conditions. This system-level standard is the IEC 61000-4-2.

System/module designers should take care to comply with the IEC 61000-4-2 system-level ESD standard. This application note shows Silicon Labs’ customers how to achieve the best possible system-level protections on board level using Silicon Labs radio chips.

2. Si4x6x Qualification Report

The Si4x6x radios' ESD robustness against the different chip level ESD standards are summarized in “Electrical Verification” of the “Qualification Report”.

The following is a brief summary from those results:

- ESD-HBM: pass up to 2 kV
- ESD-MM: pass up to 50 V for all pins, excluding RF pins if it is 200 V
- ESD-CDM: pass up to 500 V

3. Overview of IEC 61000-4-2 Standard

The IEC standard is a system level test that replicates a charged person discharging to a system in a system end user environment. The purpose of the system level test is to ensure that finished products can survive normal operation and it is generally assumed that the user of the product will not take any ESD precautions to lower ESD stress to the product.

The IEC 61000-4-2 standard defines four standard levels of ESD protection, using two different testing methodologies. Contact discharge involves discharging an ESD pulse directly from the ESD test gun that is touching the device under test. This is the preferred method of testing. However, the standard provides for an alternate test methodology known as air discharge for cases where contact discharge testing is not possible. In the air discharge test, the ESD test gun is brought close to the device under test until a discharge occurs. The standards are defined so that each level is considered equivalent – a Level 4 contact discharge of 8 kV is considered equivalent to a 15 kV air discharge.
3.1. Recommended ESD Test Bench

Figure 1. IEC 61000-4-2 Test Bench

3.2. Simulation Circuit

The IEC standard replicates a charged person discharging into a system in an uncontrolled environment. This test is performed to ensure the system will remain operational in an end user environment where no ESD stress precautions are taken.

Figure 2. Simulation Circuit of IEC 61000-4-2
3.3. IEC 61000-4-2 Test Levels

<table>
<thead>
<tr>
<th></th>
<th>Contact Discharge</th>
<th>Air Discharge</th>
</tr>
</thead>
<tbody>
<tr>
<td>Level</td>
<td>Test Voltage (kV)</td>
<td>Level</td>
</tr>
<tr>
<td>1</td>
<td>2</td>
<td>1</td>
</tr>
<tr>
<td>2</td>
<td>4</td>
<td>2</td>
</tr>
<tr>
<td>3</td>
<td>6</td>
<td>3</td>
</tr>
<tr>
<td>4</td>
<td>8</td>
<td>4</td>
</tr>
</tbody>
</table>

3.4. Pulse Waveform

Figure 3. IEC 61000-4-2 ESD Pulse Waveform
### 3.5. Peak Current of IEC 61000-4-2 ESD Standard

<table>
<thead>
<tr>
<th>Applied Voltage (kV)</th>
<th>Peak Current (A)</th>
</tr>
</thead>
<tbody>
<tr>
<td>2</td>
<td>7.5</td>
</tr>
<tr>
<td>4</td>
<td>15.0</td>
</tr>
<tr>
<td>6</td>
<td>22.5</td>
</tr>
<tr>
<td>8</td>
<td>30.0</td>
</tr>
<tr>
<td>10</td>
<td>37.5</td>
</tr>
</tbody>
</table>
4. ESD Protection Circuit Example

This section contains an example of an ESD protection circuit that can effectively suppress an IEC 61000-4-2 ESD shock.

The following passive components can be included in an effective external ESD protection circuit: series resistors, ferrites, filtering capacitors and inductors, transient voltage suppressors (e.g., TVS diodes), thyristors, varistors, polymer, etc.

The ESD protection circuit composed from these above components can block ESD currents and clamp ESD-induced high voltages. The exceeded ESD currents can be suppressed and shunted to minimize the effects of the ESD pulses in the system. It is highly recommended to place the protection circuit as close as possible to the connection point on the board where the ESD shock event can occur. This placing approach can minimize the possibility of causing further couplings of the ESD currents and voltages to the other blocks on the module.

A general I/O connector of a piece of electrical equipment can be protected with the example circuit composed with external passive components shown in Figure 4.

![Figure 4. Example for ESD Protection Circuit](image)

- J1: connection point where the ESD shock occurs (high-voltage IEC 61000-4-2 Test Pulse)
- J2: ESD-protected connection point (suppressed test signal)
- L1: series filtering inductor
- C1, C2: parallel filtering capacitors
- D1: TVS diode
- R: series resistor

The ESD shock is supposed to occur at the “J1” point. The “L-C” low-pass filtering section suppresses the fast ESD shock signal; the “L1” inductor can block the large currents, while the “C1” and “C2” capacitors can limit the high voltage induced by the transient fast current spike.

The “D1” TVS diode can be effectively used for suppressing the fast ramped-up ESD signals and plenty of these kinds of diodes are available on the market from different manufacturers (specified for assisting equipment to pass IEC 61000-4-2, even level 4 testing).

The optimum values for the components and even the optimum structure (i.e., it might not be necessary to use all of the shown components in Figure 4) depend on the level of the ESD signal, board layout, and on the termination at the “J2” point.

It is possible to select the filtering element values in a way where the largest suppression can be achieved at the GHz region, since the ramp-up time of the fast ESD signal is around 1 ns, as shown in Figure 3.
5. Waveform Measurements as IEC 61000-4-2 Standard

Silicon Labs performed waveform measurements with the following setup:
- IEC 61000-4-2 ESD standard test bench setup
- IEC 61000-4-2 ESD standard test signals
- Direct contact waveform measurements from the IEC 61000-4-2 test signal
- Contact waveform measurements with applying an example ESD protection circuit

This section illustrates how the waveforms look before (direct measurement of IEC 61000-4-2 test signal) and after an example ESD protection circuit. In addition, this section demonstrates the effectiveness of the protection circuit.

The TVS diode used in the example protection circuit ("D1") is: SESD0402X1UN.

The ESD protection circuit was realized on a small PCB that only included the elements shown in Figure 4.

The following figures show the measured waveforms with different conditions such as voltage of the test signal, different elements mounted on the ESD protection board, different element values, and etc. The conditions are identified in each figure caption.

Figure 5. IEC 61000-4-2 Test Signal, +2 kV, without Protection
Figure 6. IEC 61000-4-2 Test Signal, +8 kV, without Protection

Figure 7. IEC 61000-4-2 Test Signal, +2 kV, TVS Diode Mounted
Figure 8. IEC 61000-4-2 Test Signal, +2 kV, TVS Diode and C1 = 2 nF Mounted

Figure 9. IEC 61000-4-2 Test Signal, +8 kV, TVS Diode and C1 = 2 nF Mounted
Figure 10. IEC 61000-4-2 Test Signal, +8 kV, TVS Diode and C1 = 2 nF, C2 = 33 pF Mounted

Figure 11. IEC 61000-4-2 Test Signal, +8 kV, TVS Diode and C1 = 2 nF, C2 = 33 pF, R = 15 Ω Mounted
Figure 12. IEC 61000-4-2 Test Signal, +8 kV, 2 TVS Diodes and C1 = 2 nF, C2 = 33 pF, R = 15 Ω Mounted

Figure 13. IEC 61000-4-2 Test Signal, +2 kV, 2 TVS Diodes and C1 = 2 nF, C2 = 33 pF, R = 15 Ω Mounted
Figure 14. IEC 61000-4-2 Test Signal, +2 kV, 2 TVS Diodes and C1 = 2 nF, R = 15 Ω Mounted, Extended Time Scale
Figure 15. IEC 61000-4-2 Test Signal, +2 kV, 2 TVS Diodes and C1 = 2 nF, R = 15 Ω Mounted

Figure 16. IEC 61000-4-2 Test Signal, +2 kV, 2 TVS Diodes and C1 = 2 nF, R = 15 Ω Mounted
6. ESD Demonstration on Silicon Labs’ Reference Design

Silicon Labs has also performed some extra measurements to demonstrate the effectiveness of the example ESD protection circuit. The measurement setup is as follows:

- HW: Silicon Labs Wireless Motherboard with Si4x6x RF Pico Board connected
- Contact stressing the HW with IEC 61000-4-2 test signal directly
- Contact stressing the HW with IEC 61000-4-2 test signal, but via the ESD protection circuit
- Contact stressing points on the HW: single-row via test points of the RF Pico Board (see Figure 17)
  - ESCL pin: non-directly connected trace with the RF chip
  - VDD pin: power supply, direct connection with the RF chip
  - NSEL: directly connected trace with the RF chip
  - RF port: RF antenna connection point, not test point, extra notes in Section 8.

Note: Contact stressing the HW at these connection points is a very worst-case event compared to a real application where these points are typically not directly led out on the final module.

![Wireless Motherboard with RF Pico Board Connected](image-url)

**Figure 17. Wireless Motherboard with RF Pico Board Connected**
The ESD protection circuit applied during these demonstration measurements is shown in Figure 18. This circuit was realized in a small PCB, separated from the RF Pico Board and Wireless Motherboard. Note that the example of ESD protection circuit shown below can be applied on any general design (i.e., not only Si4x6x-based designs) excluding on the RF or antenna ports.

![Figure 18. ESD Protection Circuit](image)

The results are summarized in Table 1.

<table>
<thead>
<tr>
<th>Stressed Pin</th>
<th>Presence of Protection Circuit</th>
<th>IEC 61000-4-2 Test Signal Maximum Voltage</th>
</tr>
</thead>
<tbody>
<tr>
<td></td>
<td></td>
<td>+2 kV</td>
</tr>
<tr>
<td>ESCL</td>
<td>NO</td>
<td>FAIL</td>
</tr>
<tr>
<td></td>
<td>YES</td>
<td>PASS</td>
</tr>
<tr>
<td>NSEL</td>
<td>NO</td>
<td>FAIL</td>
</tr>
<tr>
<td></td>
<td>YES</td>
<td>PASS</td>
</tr>
<tr>
<td>VDD</td>
<td>NO</td>
<td>PASS</td>
</tr>
<tr>
<td></td>
<td>YES</td>
<td>PASS</td>
</tr>
<tr>
<td>RF port</td>
<td>NO</td>
<td>FAIL</td>
</tr>
<tr>
<td></td>
<td>YES</td>
<td>PASS</td>
</tr>
</tbody>
</table>
7. Layout Suggestions

The following layout suggestions are recommended to ensure the possible best immunity against any ESD shock:

- Keep the antenna far from any connector that has potential risk for ESD shock.
- Route traces far from the antenna; this helps to avoid any couplings between the traces and antenna that prevents possible latch-up issues.
- Always try to ensure good grounding in terms of RF (i.e., use large, continuous GND copper pouring on the PCB with plenty of stitching vias).
- Try to route the potential ESD risk traces (i.e., traces connected to the potential risk connectors) far from the RF section.
- Place the ESD protection circuit as close to the ESD shock point as possible. In this way, the further couplings of the ESD shock signals can be minimized.

The application note, “AN629: Layout Design Guide”, also includes some RF-related recommendations. The proper design of the PCB layout can minimize the possibility of any signal couplings and avoid the risk of failing against an ESD shock.
8. Antenna Protection

Due to the high operating frequency (RF) of the protected port of an ESD protection circuit, the most important considerations are the following:

- Do not use parallel capacitors since they can de-tune the RF antenna. The RF antenna is also frequency dependent, so a maximum 0.5…1.5 pF capacitors are allowed in the sub-GHz region).
- Do not use series inductors since they also de-tune the RF antenna. However, series bypass (bypass at the operating frequency) capacitor can be used.
- Do not use series resistors since they bring extra loss into the RF front-end and therefore cause RF power efficiency degradation.
- Take care about the parasitics of the selected TVS diode (or any other suppressor). Select fast, low capacitance devices to minimize the de-tuning of the RF antenna.
- Parallel shunt from RF to GND inductors can be used to suppress any low frequency noises. The value of the parallel inductor has to be the same as the “RF choke inductor” (i.e., the inductor has to show high impedance at the operating RF frequency that is equal with SRF, self-resonant-frequency, of the chip inductor).

Based on the additional RF port-related considerations described above, Figure 19 shows a generic suggested ESD protection circuit for the RF antenna port. Note that the example of ESD protection circuit for RF and antenna ports shown below can be applied on any general RF design (i.e., not only Si4x6x-based designs).

![Figure 19. ESD Protection Circuit for RF Antenna Port](image)

Recommended element values are summarized in Table 2. The ESD immunity measurement results on the RF antenna port are included in Table 1 in section 6.
Examples for the recommended TVS diodes: SESD0402X1UN, ESD101-B1-02EL, etc.

If it is not possible to select TVS diodes with the low capacitance values listed in the C2 row of Table 2 above, then the following network implementation can be used as an additional ESD protection circuit in the RF path. This approach creates a 3-element, low-pass PI filter structure. So, basically, the additional capacitance of the D1 and D2 TVS diodes is resonated out by the series L2 inductor at the desired RF frequency.

Table 2. Suggested Element Values for the Antenna Protection Circuit

<table>
<thead>
<tr>
<th>Element</th>
<th>RF Frequency Band</th>
<th>Value</th>
</tr>
</thead>
<tbody>
<tr>
<td>L1</td>
<td>310-510 MHz</td>
<td>270 nH</td>
</tr>
<tr>
<td></td>
<td>780-930 MHz</td>
<td>120 nH</td>
</tr>
<tr>
<td></td>
<td>2.4 GHz</td>
<td>22 nH</td>
</tr>
<tr>
<td>C1</td>
<td>310-510 MHz</td>
<td>270 pF</td>
</tr>
<tr>
<td></td>
<td>780-930 MHz</td>
<td>68 pF</td>
</tr>
<tr>
<td></td>
<td>2.4 GHz</td>
<td>10 pF</td>
</tr>
<tr>
<td>C2</td>
<td>310-510 MHz</td>
<td>N.M. but can go up to 1.5 pF</td>
</tr>
<tr>
<td></td>
<td>780-930 MHz</td>
<td>N.M. but can go up to 0.5 pF</td>
</tr>
<tr>
<td></td>
<td>2.4 GHz</td>
<td>N.M. but should be kept &lt; 0.2 pF</td>
</tr>
</tbody>
</table>
| D1      |                   | Note: The purpose of these TVS diodes is to suppress the ESD signal. The selection of fast, low-capacitance devices is recommended.
| D2      |                   |               |

Figure 20. Additional ESD Protection Circuit in the RF Path
9. POR when ESD Shock Occurs

This section highlights what happens if an ESD shock occurs that affects the operation of an Si4x6x device. In most cases, when an ESD shock occurs, the radio chip is not damaged, but Power-On-Reset (POR) occurs. This means that the radio chip can be re-configurable after the POR event and no hard impact results. By default, the monitoring of the GPIO-1 signal results in detection of the POR, after which the chip settings can be sent to the radio chip to get the radio properly working again.

Figure 21 shows the GPIO-1 signal during ESD shock. As shown in the figure, POR occurs and, when the GPIO-1 signal is high again, the radio can be configurable again by software.

![Figure 21. GPIO-1 Signal during ESD Event](image)

So, in most cases after an ESD shock, the radio chip can be used again, it only needs to be re-configured by software. To accomplish this task, the GPIO-1 signal has to be monitored to make sure that the POR occurred after an ESD event.

Silicon Labs also monitored the current consumption of the RF chip during ESD shock. The current consumption never exceeded the TX current consumption value.
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